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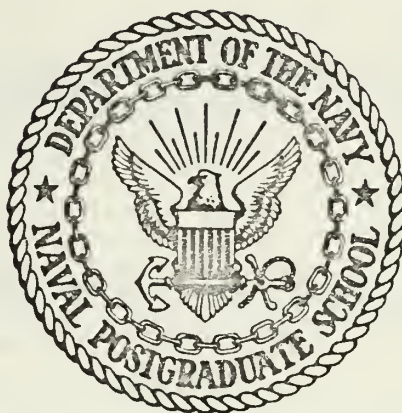
STABILITY OF A TROPICAL MODEL INCLUDING  
SHEAR, SURFACE FRICTION AND CISK HEATING

Terry Gene Robertson

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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

STABILITY OF A TROPICAL MODEL INCLUDING SHEAR,  
SURFACE FRICTION AND CISK HEATING

by

Terry Gene Robertson

Thesis Advisor:

R.T. Williams

March 1973

*Approved for public release; distribution unlimited.*

T153553



Stability of a Tropical Model Including Shear,  
Surface Friction and CISK Heating

by

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MASTER OF SCIENCE IN METEOROLOGY

from the

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March 1973



## ABSTRACT

The structure of barotropically unstable disturbances in the tropics is studied with a two-level quasi-geostrophic model. An Ekman layer is attached to the lower boundary. The equations are linearized and the most unstable mode is found numerically by use of the initial value technique. CISK heating, horizontal friction and shear are introduced to give more realistic solutions. Computations are made for two shear zone wind profiles. The first is represented by  $\bar{U}_1 = \bar{U}_3 = -U_0 \tanh y/y_0$  and the second is a mirror reflection of the first and is given by  $\bar{U}_3 = -\bar{U}_1$ . The model is run for 142 days after which growth rates are determined as a function of the non-dimensional wave number  $ky_0$ . The associated phase angles and amplitudes for the wave numbers with maximum growth rates are given. The solutions with heating do not have a strongly preferred mode of maximum growth.





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TABLE OF SYMBOLS AND ABBREVIATIONS

$A_e$	Vertical Eddy Viscosity
$A_H$	Horizontal Eddy Viscosity
$\beta$	Derivative of Coriolis parameter at $y = 0$
$c_p$	Specific heat at constant pressure
$f_o$	Coriolis parameter at $y = 0$
$g$	Gravity
$\omega$	$dp/dt$
$\psi$	$gz/f_o$
$R$	Gas constant for dry air
$\rho$	Density
$\bar{T}$	Average temperature from the standard atmosphere
$\sigma$	$(R^2\bar{T}/p^2g) (\partial\bar{T}/\partial z + g/c_p)$
$\zeta$	$\nabla^2\psi$
$z$	Height
$Q$	Heating added per unit mass
$\nabla^4$	Bi-harmonic operator $(\nabla^2)^2$
$\alpha$	Wind inflow angle



## ACKNOWLEDGEMENTS

The author wishes to express his deep appreciation to Dr. Roger Terry Williams for his guidance, understanding, and counsel in the preparation of this thesis and to Dr. C. P. Chang and Dr. R. L. Elsberry for reading the thesis and making useful comments.

The author is also thankful to Captain Thomas Kent Schminke and Commander Robert L. Newman who allowed their models to be modified for the experiments conducted.

All computations were made on the IBM 360 computer at the W. R. Church Computer Center, Naval Postgraduate School, Monterey, California. The author wishes to extend his gratitude to the personnel at the computer center for their assistance and cooperation.



## I. INTRODUCTION

Synoptic scale disturbances in the tropical atmosphere have been recognized for a long time (Palmer 1951, Riehl 1954). This paper is concerned with wave disturbances that occur in the lower troposphere and makes no distinction between easterly waves and equatorial waves. Starr and Wallace (1964) showed that in the lower troposphere these disturbances have a "cold core" structure; the rising air is cooler than the air which is subsiding. Warm core structures at higher levels with significant correlations between temperature and vertical velocity have been found by Chang et al. (1970) and Nitta (1970). Vertical velocities associated with these disturbances in general are rising air to the east of the wave axis and subsidence to the west (Yanai and Nitta, 1967).

The energy source for these waves is not known. Baroclinic instability is unlikely because of the smallness of the Coriolis parameter. Charney (1963) performed a scale analysis which indicated that, in the absence of condensation, large-scale motions in the tropics are governed by the barotropic vorticity equation. Charney (1963) suggested that easterly waves arise from barotropic instability. The spectral analysis of Wallace and Chang (1969) indicate a conversion of kinetic energy from the mean flow to the disturbance.





A third possible energy source for these disturbances is latent heat of condensation.

This mechanism is consistent with observations of warm core structures at upper levels (Chang et al. 1970). This heating has been parameterized by Ooyama (1964), Charney and Eliassen (1964), and Kuo (1965) in such a manner that the condensation heating is proportional to the convergence of moisture in the Ekman layer. This leads to a simple instability which is called Conditional Instability of the Second Kind (CISK). Yamasaki (1969) studied the influence of CISK on linearized disturbances in an atmosphere with vertical shear. The solutions displayed many features that are observed in actual tropical wave disturbances. Holton (1971) has obtained similar results with a model that contains a moving heat source and vertical wind shear. These studies strongly suggest that the tropical disturbances are driven by condensation heating. It is known that the CISK mechanism must have a pre-existing disturbance to organize the convective elements before CISK can operate. This pre-existing disturbance could arise from barotropic instability as was demonstrated by Bates (1970). Kuo (1949) examined the stability characteristics of a barotropic zonal current and found that instability is possible only when the absolute vorticity gradient reverses sign in the region.

The purpose of this thesis is to extend the work done by Williams et. al. (1971) to include cases with CISK heating, horizontal friction and vertical shear. Since the Williams



et al. (1971) paper is referenced many times, it will hereafter be referred to as WSN.



## II. THE FORECAST EQUATIONS

The quasi-geostrophic prediction equations will be used as the forecast equations following WSN. It is recognized that the quasi-geostrophic approximation is not very accurate near the Equator, but Matsuno (1966) has shown with a barotropic model that quasi-geostrophic motions are identifiable near the Equator if the wavelength is not too long. Yamasaki (1969) has found that the error is small at 20 degrees latitude in a study with a baroclinic model.

The quasi-geostrophic equations are simplified through the introduction of a two-level model which was also used by Bates (1970). The equations are linearized and solved numerically by the initial value technique. The growth rates and wave structures are then computed.

A simple two-level model is constructed by dividing the atmosphere into four layers with a constant pressure differential of  $\Delta p/2$  (Fig. 1), numbered 0 to 4 from top to bottom. The boundary condition at  $p = p_t$  is  $\omega_0 = 0$ , which prohibits vertical propagation of energy. Charney (1969) has shown that such energy propagation is unlikely. At  $p = p_0$  the boundary condition is  $\omega = \omega_e$  where  $\omega_e$  is the frictionally induced  $\omega$  at the top of the Ekman layer. Charney and Eliassen (1949) derived the following expression for  $\omega_e$

$$\omega_e = -\rho_4 g \left( \frac{A_e}{2f_0} \right)^{1/2} \sin 2\alpha\zeta_4 \quad , \quad (2.1)$$



where  $A_e$  is the kinematic eddy viscosity,  $\alpha$  is the surface inflow angle, and  $\zeta_4$  is the surface geostrophic vorticity.

p		Level
$p_t$	$\omega=0$	0
	$\psi_1$	1
$p_t + \Delta p$	$\omega_2$	2
	$\psi_3$	3
$p_o$	$\omega=\omega_e$	4

Fig. 1 Two-level prediction model

It has been shown by Holton et al. (1971) and Chang (1973) that this expression is reasonably valid as far equatorward as 10 degrees, but may be invalid when close to the Equator or south of the ITCZ. The surface geostrophic vorticity can be approximated by

$$\zeta_4 \approx \zeta_3 = \nabla^2 \psi_3 . \quad (2.2)$$

The quasi-geostrophic vorticity equation in pressure coordinates with horizontal eddy diffusion is

$$\frac{\partial}{\partial t} \nabla^2 \psi + \text{lkx} \nabla \psi \cdot \nabla (\nabla^2 \psi) + \beta_o \frac{\partial \psi}{\partial x} - f_o \frac{\partial \omega}{\partial p} = A_H \nabla^4 \psi . \quad (2.3)$$

Observe that when  $\omega = 0$  and  $A_H = 0$ , (2.3) becomes the barotropic vorticity equation which is sufficient to describe the main instability.





Apply this equation at levels 1 and 3 which gives

$$\frac{\partial}{\partial t} \nabla^2 \psi_1 + kx \nabla \psi_1 \cdot \nabla (\nabla^2 \psi_1) + \beta_0 \frac{\partial \psi_1}{\partial x} - f_0 \frac{\omega_2}{\Delta p} = A_H \nabla^4 \psi_1 \quad , \quad (2.4)$$

$$\frac{\partial}{\partial t} \nabla^2 \psi_3 + kx \nabla \psi_3 \cdot \nabla (\nabla^2 \psi_3) + \beta_0 \frac{\partial \psi_3}{\partial x} - f_0 \frac{(\omega_4 - \omega_2)}{\Delta p} = A_H \nabla^4 \psi_3 \quad . \quad (2.5)$$

If it is desired to stop at some intermediate point, say the tropopause, rather than to include the entire atmosphere, smaller layers could be used.

Next consider the quasi-geostrophic first law of thermodynamics in the form

$$\frac{\partial}{\partial t} \frac{\partial \psi}{\partial p} + kx \nabla \psi \cdot \left( \frac{\partial \psi}{\partial p} \right) + \frac{\sigma}{f_0} \omega = \frac{-u^2 K Q_2}{2f_0} \quad , \quad (2.6)$$

where

$$\sigma = \frac{R^2 \bar{T}}{p^2 g} \left[ \frac{\partial \bar{T}}{\partial z} + \frac{g}{C_p} \right] \quad , \quad (2.6a)$$

and  $\bar{T}$  is the temperature obtained from the standard atmosphere.

The heating follows the formulation of Ooyama (1964), Charney and Eliassen (1964), and Kuo (1965), i.e., the condensation heating is proportional to the convergence of moisture in the Ekman layer. The form used was given by Ogura (1964)



$$Q_2 = \frac{1}{2} \frac{C_p \bar{T}}{\bar{\theta}} \frac{\partial \bar{\theta}}{\partial p} \eta \omega_4 , \quad (2.7)$$

where  $\eta$  is a non-dimensional parameter. This relationship is used in both rising and subsiding air since a Fourier expansion in  $x$  is used; therefore the amplitude of heating is divided by two.

When (2.6) is applied at level 2 the result is

$$\frac{\partial}{\partial t} (\psi_1 - \psi_3) + kx \nabla \left( \frac{\psi_1 + \psi_3}{2} \right) \cdot \nabla (\psi_1 - \psi_3) - \frac{\Delta p \sigma_2 \omega_2}{f_o} = \frac{-\mu^2 K Q_2}{2f_o} . \quad (2.8)$$

Define the following quantities

$$\psi_M = \frac{\psi_1 + \psi_3}{2} , \quad (2.9)$$

$$\psi_T = \frac{\psi_1 - \psi_3}{2} , \quad (2.10)$$

which implies that

$$\psi_1 = \psi_M + \psi_T , \quad (2.11)$$

$$\psi_3 = \psi_M - \psi_T . \quad (2.12)$$

Here  $\psi_T$  is proportional to the layer thickness and is therefore a measure of the mean temperature in the layer. Use these definitions, add (2.4) and (2.5) and divide the result by two, which gives



$$\begin{aligned}
& \frac{\partial}{\partial t} \nabla^2 \psi_M + kx \nabla \psi_M \cdot \nabla (\nabla^2 \psi_M) + kx \nabla \psi_T \cdot \nabla (\nabla^2 \psi_T) \\
& + \beta_0 \frac{\partial \psi_M}{\partial x} - \frac{f_0 \omega_4}{2\Delta p} = A_H \nabla^4 \psi_M .
\end{aligned} \tag{2.13}$$

For the second forecast equation, subtract (2.5) from (2.4) and eliminate  $\omega_2$  with the use of (2.8) which gives

$$\begin{aligned}
& \frac{\partial}{\partial t} (\nabla^2 - \mu^2) \psi_T + kx \nabla \psi_M \cdot \nabla (\nabla^2 - \mu^2) \psi_T + kx \nabla \psi_T \cdot \nabla (\nabla^2 \psi_M) \\
& + \beta_0 \frac{\partial \psi_T}{\partial x} + \frac{f_0 \omega_4}{2\Delta p} = \frac{-\mu^2 K Q_2}{2f_0} + A_H \nabla^4 \psi_T ,
\end{aligned} \tag{2.14}$$

where

$$\mu^2 = \frac{2f_0^2}{p^2 \sigma_2} \tag{2.14a}$$

These are the prediction equations for the model. To linearize the equations, the flow is separated into an east-west current that varies only in  $y$ , and a small departure from this flow. Thus it is possible to treat waves in  $x$  independently and the fields can be defined as follows

$$\psi_M = E(y) + A(y,t) \cos kx + B(y,t) \sin kx , \tag{2.15}$$

$$\psi_T = F(y) + C(y,t) \cos kx + D(y,t) \sin kx , \tag{2.16}$$



where  $k$  is the  $x$  wave number. The coefficients  $A$  through  $D$  are Fourier amplitudes of the disturbance and  $E$  and  $F$  are the coefficients of the mean zonal fields.

Substitute the expressions for  $\psi_M$  and  $\psi_T$  into (2.13), separate the various sine and cosine terms, and neglect all products of the quantities  $A$  through  $D$ . Equate the coefficients of the cosine terms which gives

$$\begin{aligned} \frac{\partial}{\partial t} \left( \frac{\partial^2 A}{\partial y^2} - Ak^2 \right) &= k \left[ \frac{\partial E}{\partial y} \frac{\partial^2 B}{\partial y^2} + \frac{\partial F}{\partial y} \frac{\partial^2 D}{\partial y^2} - \frac{\partial^3 E}{\partial y^3} B - \frac{\partial^3 F}{\partial y^3} D \right. \\ &\quad \left. - k^2 \left( \frac{\partial E}{\partial y} B + \frac{\partial F}{\partial y} D \right) \right] - \beta_0 Bk - K \left( \frac{\partial^2}{\partial y^2} - k^2 \right) (A - C) \\ &\quad + A_H \left( \frac{\partial^4 A}{\partial y^4} - 2k^2 \frac{\partial^2 A}{\partial y^2} + k^4 A \right) , \end{aligned} \quad (2.17)$$

The sine terms give

$$\begin{aligned} \frac{\partial}{\partial t} \left( \frac{\partial^2 B}{\partial y^2} - Bk^2 \right) &= k \left[ - \frac{\partial E}{\partial y} \frac{\partial^2 A}{\partial y^2} - \frac{\partial F}{\partial y} \frac{\partial^2 C}{\partial y^2} + \frac{\partial^3 E}{\partial y^3} A + \frac{\partial^3 F}{\partial y^3} C \right. \\ &\quad \left. + k^2 \left( \frac{\partial E}{\partial y} A + \frac{\partial F}{\partial y} C \right) \right] + \beta_0 Ak - K \left( \frac{\partial^2}{\partial y^2} - k^2 \right) (B - D) \\ &\quad + A_H \left( \frac{\partial^4 B}{\partial y^4} - 2k^2 \frac{\partial^2 B}{\partial y^2} + k^4 B \right) . \end{aligned} \quad (2.18)$$





Repeat the procedure for (2.14) for the cosine terms which gives

$$\begin{aligned}
 \frac{\partial}{\partial t} \left( \frac{\partial^2 C}{\partial y^2} - Ck^2 - C\mu^2 \right) &= k \left[ \frac{\partial E}{\partial y} \frac{\partial^2 D}{\partial y^2} + \frac{\partial F}{\partial y} \frac{\partial^2 B}{\partial y^2} - \frac{\partial E}{\partial y} D(k^2 + \mu^2) \right. \\
 &\quad \left. - \frac{\partial F}{\partial y} B(k^2 - \mu^2) - \frac{\partial^3 E}{\partial y^3} D - \frac{\partial^3 F}{\partial y^3} B \right] - \beta_0 Dk \\
 &\quad + (K - S) \left( \frac{\partial^2}{\partial y^2} - k^2 \right) (A - C) + A_H \left( \frac{\partial^4 C}{\partial y^4} - 2k^2 \frac{\partial^2 C}{\partial y^2} + k^4 C \right) ,
 \end{aligned} \tag{2.19}$$

The results for the sine terms are

$$\begin{aligned}
 \frac{\partial}{\partial t} \left( \frac{\partial^2 D}{\partial y^2} - Dk^2 - D\mu^2 \right) &= k \left[ \frac{\partial E}{\partial y} C(k^2 + \mu^2) + \frac{\partial F}{\partial y} A(k^2 - \mu^2) \right. \\
 &\quad \left. - \frac{\partial E}{\partial y} \frac{\partial^2 C}{\partial y^2} - \frac{\partial F}{\partial y} \frac{\partial^2 A}{\partial y^2} + \frac{\partial^3 F}{\partial y^3} A + \frac{\partial^3 E}{\partial y^3} C \right] + \beta_0 Ck \\
 &\quad + (K - S) \left( \frac{\partial^2}{\partial y^2} - k^2 \right) (B - D) + A_H \left( \frac{\partial^4 D}{\partial y^4} - 2k^2 \frac{\partial^2 D}{\partial y^2} + k^4 D \right) ,
 \end{aligned} \tag{2.20}$$

where

$$K = \frac{f_0 g}{2R\theta} \left( \frac{A_M}{f_0} \right)^{1/2} , \tag{2.21}$$



and

$$S = \frac{g}{\theta} \frac{\eta}{|\theta|} \frac{\partial \bar{\theta}}{\partial p} p_o \left( \frac{A_M}{f_o} \right)^{1/2} \frac{1}{f_o} . \quad (2.22)$$

These are the same equations used by WSN except that in their equations  $F = 0$ ,  $\eta = 0$ , and  $A_H = 0$ .

It is necessary to derive the computational equation for vertical motion beginning with

$$\omega_2 = \frac{2}{\Delta p \sigma} \left[ \frac{\partial \psi_T}{\partial t} + u_m \frac{\partial \psi_T}{\partial x} + v_m \frac{\partial \psi_T}{\partial y} + \frac{KQ_2}{2f_o} \right] , \quad (2.23)$$

where

$$u_m = - \frac{1}{f_o} \frac{\partial \psi_M}{\partial y} , \quad (2.24)$$

$$v_m = \frac{1}{f_o} \frac{\partial \psi_M}{\partial x} . \quad (2.25)$$

Substitute equations (2.24), (2.25) and (2.16) into (2.23), collect terms, and again neglect all products of A through D which gives

$$\begin{aligned} \omega_2 = \frac{2}{\Delta p \sigma} \left\{ \cos kx \left[ \frac{\partial C}{\partial t} - \frac{k}{f_o} \left( \frac{\partial E}{\partial y} D - \frac{\partial F}{\partial y} B \right) \right] \right. \\ \left. + \sin kx \left[ \frac{\partial D}{\partial t} + \frac{k}{f_o} \left( \frac{\partial E}{\partial y} C - \frac{\partial F}{\partial y} A \right) \right] + \frac{\partial F}{\partial t} + \frac{KQ_2}{2f_o} \right\} . \end{aligned} \quad (2.26)$$



Both the disturbance and the average vertical motion are given by this equation. The prediction equations and the vertical motion equations are now in the form to be used in the model.



### III. BOUNDARY CONDITIONS AND FINITE DIFFERENCING SCHEME

The finite difference scheme that was used is illustrated below with a sample variable  $M_i$ :

$$\frac{\partial M}{\partial y} = \frac{1}{2H} (M_{i+1} - M_{i-1}), \quad (3.1)$$

$$\frac{\partial^2 M}{\partial y^2} = \frac{1}{H^2} (M_{i+1} - 2M_i + M_{i-1}), \quad (3.2)$$

$$\frac{\partial^3 M}{\partial y^3} = \frac{1}{2H^3} [(M_{i+2} - 2M_{i+1} - M_i) - (M_i - 2M_{i-1} + M_{i-2})]. \quad (3.3)$$

where  $i$  is the grid index and  $H$  is the distance between grid points.

Centered time differences were used for all quantities except those involving friction and heating. The friction and heating terms were computed at time  $(t - \Delta t)$ . Initially a forward time step was used. The second order equations for time tendencies were solved by the exact method of Richtmyer (1957, p. 101).

Yanai and Nitta (1968a) studied the problem of using finite difference approximations to solve dynamic instability problems of non-divergent barotropic currents. They showed that for either symmetric or anti-symmetric zonal currents, the exact boundary conditions can be replaced by





placing rigid boundary conditions at a distance equal to one-half the width of the shearing wind belt. Therefore rigid boundaries are placed at  $y = -W/2$  and  $y = W/2$ , where  $W$  is the total width of the computational field. Except for the  $E$  and  $F$  fields, all variables have the boundary condition  $A = B = C = D = 0$  at  $y = \pm W/2$ . Second derivatives that are required on the boundary are set equal to zero.





Fig. 2 Mean wind profile  $\bar{U} = -U_0 \tanh y/y_0$



#### IV. WIND PROFILE AND INITIAL CONDITIONS

WSN investigated the structure of tropical disturbances using a similar model and the wind profile ( $U = -U_0 \tanh y/y_0$ ). It is proposed to expand on that paper to include a sinusoidal profile for an initial disturbance and a thermal wind field which will be a mirror image of the mean wind field used by WSN.

If the waves are to grow, the zonal wind profile must be barotropically unstable. Charney (1963) suggested that a shear zone could be formed by the transport of angular momentum from different regions. This would occur when the Intertropical Convergence Zone is shifted away from the Equator. The unstable profile chosen to represent this is

$$\bar{U}_1 = \bar{U}_3 = -U_0 \tanh y/y_0, \quad (4.1)$$

which is illustrated in Figure 2. To represent a thermal wind field the unstable profile is

$$\bar{U}_1 = -\bar{U}_3 = U_0 \tanh y/y_0. \quad (4.2)$$

Lipps (1970) has used the profile represented by (4.1) in an inviscid study of barotropic instability in the tropics. This wind field is anti-symmetric with respect to the Intertropical Convergence Zone, located at  $y = 0$ .



For the experiments which have the wind profile (4.1), a range of non-dimensional wave numbers ( $ky_0$ ) from 0.10 to 3.00 will be used. This wide range of wave numbers is necessary because it is uncertain which wave number will be the most unstable mode. Those experiments with the (4.2) wind profile will be run over a range of 0.10 to 1.20. One experiment with the latter wind profile containing CISK heating was run over a wave number range of 0.10 to 3.00.

$\psi_M$  is introduced into the model as a sinusoidal disturbance in  $y$  and  $\psi_T$  grows from zero as a result of the Ekman friction term. CISK heating is added which greatly increases the growth rates of all fields, particularly the short waves. Horizontal friction is also added. This represents a mixing of the smaller scale waves and smooths out perturbations in the vertical velocity field. Thus at time  $t = 0$

$$A = \sin \frac{\pi y}{W} \quad (4.3)$$

$$B = 0 \quad (4.4)$$

$$C = 0 \quad (4.5)$$

$$D = 0 \quad (4.6)$$

$$E = f_0 U_0 y_0 \ln[\cosh (y/y_0)] \quad \text{or} \quad 0 \quad (4.7)$$

$$F = -f_0 U_0 y_0 \ln[\cosh (y/y_0)] \quad \text{or} \quad 0 \quad (4.8)$$





## V. COMPUTATIONAL PROCEDURE

The following constants were used in all computations except those related to heating and friction which were zero if the heating and/or the friction are neglected:

$p_o$	=	100 centibars,
$y_o$	=	400 or 200 or 100 kilometers,
$W$	=	4000 kilometers,
$U_o$	=	10 meters per second,
$f_o$	=	$5 \times 10^{-5}$ per second,
$\sigma$	=	0.4 meters per second squared per centibar squared,
$\beta$	=	0.0 or $2.29 \times 10^{-11}$ per meter per second,
$\Delta p$	=	50 centibars,
$A_e$	=	10 meters per second squared,
$A_H$	=	$1 \times 10^5$ meters per second squared,
$\alpha$	=	22.5 degrees,
$\mu^2$	=	$2.49 \times 10^{-12}$ per meter squared,
$H$	=	50 or 25 or 12.5 kilometers,
$\Delta t$	=	1.0 or 0.5 or 0.25 hours,
$\eta$	=	2.0 or 1.0,
$\partial \bar{\theta} / \partial p$	=	-0.6 degrees per centibar.

A forecast period of 142 days was used so that the most unstable mode would have reached the maximum growth rate. For most cases, it was found that the growth rate at 110 days was the same as the growth rate at the longer period.



WSN introduced a random disturbance into the  $\psi_M$  field. It was found that by using a sinusoidal profile for the disturbance, similar growth rates were obtained except in the cases where heating was added. The sinusoidal profile was used as the disturbance field for all experiments with variations of  $\bar{U}$ ,  $\beta$ , CISK heating, horizontal and surface friction, and the non-dimensional wave number ( $ky_0$ ). Growth rates were then computed by assuming the amplitude could be written as

$$a_1 = a_0 \exp(nU_0/y_0) t_1, \quad (5.1)$$

$$a_2 = a_0 \exp(nU_0/y_0) t_2, \quad (5.2)$$

where  $n$  is the growth rate and  $a_0$  is a constant. If the ratio  $a_2/a_1$  is formed, the growth rate can be shown to be

$$n = \frac{y_0 \ln(a_2/a_1)}{U_0(t_2 - t_1)}. \quad (5.3)$$

The dimensional doubling time is

$$T = \frac{y_0 \ln 2}{nU_0}. \quad (5.4)$$



## VI. RESULTS

A series of experiments were conducted over a wide variety of conditions. The total distance over the grid was 4000 km. A grid mesh size of 50 km and a time step of 1.0 hours was used for all experiments except two cases. In one case a grid mesh of 25 km with a 0.5 hour time step was used and in the other case a grid mesh of 12.5 km and a 0.25 hour time step was used.

The more important experiments are given in Table 1 as a function of  $\bar{U}$ ,  $\beta$ , heat, friction, and  $ky_0$ . The growth rate  $n$  is also given. The table shows whether or not CISK heating and horizontal friction were included for each experiment. All experiments given in Table 1 included surface friction. For each experiment, calculations were made to determine the non-dimensional growth rate as a function of the non-dimensional wave number  $ky_0$  so that the results could be compared to those obtained by WSN. The value of  $ky_0$  that was associated with the maximum growth rate is shown in the table.

It should be mentioned that the value used for the non-dimensional heating parameter  $\eta$  was too large. A more realistic value for  $\eta$  would have been 1.0 instead of 2.0. Test runs were made for experiments 1 through 4 with  $\eta = 1.0$  and in all cases, the growth rates were reduced to about one-third the value obtained with the larger value of  $\eta$ .



Table 1. Compilation of numerical experiments

Exp	$\bar{U}$	$\beta$	$n$	Heating	Friction	$ky_0$
1	$\bar{U}_1 = \bar{U}_3$	0	0.770	Yes	No	0.40
2	$\bar{U}_1 = \bar{U}_3$	$2.29 \times 10^{-11}$	0.730	Yes	No	0.40
3	$\bar{U}_1 = \bar{U}_3$	0	0.520	Yes	Yes	0.40
4	$\bar{U}_1 = \bar{U}_3$	$2.29 \times 10^{-11}$	0.520	Yes	Yes	0.40
5	$\bar{U}_1 = -\bar{U}_3$	0	0.283	No	No	0.65
6	$\bar{U}_1 = -\bar{U}_3$	0	0.790	Yes	No	1.10

Experiment 1 was run with the (4.1) wind profile and included CISK heating and surface friction. The beta term and horizontal friction were excluded. Garcia (1956) found that the shear zone profile (4.1) is barotropically unstable when  $0 < ky_0 < 1$ . Betchov and Criminale (1967) computed the eigensolutions for this profile throughout this range and found the maximum instability at  $ky_0 = 0.45$  which agreed with the results of WSN. The wave number of maximum instability (0.40) agrees quite closely with that value but the growth rate ( $n = 0.770$ ) is much greater than the value obtained by WSN ( $n = 0.153$ ) even when the smaller value of  $n$  was used. Figure 3 contains the growth rate profile for the full range of wave numbers. The maximum growth rate corresponds to a doubling time of 0.42 days and a wavelength of 6280 km. The sharp irregularities between 0.10 and 1.00





arise because the wave number increment in that region is 0.10 as compared to 0.50 between 1.00 and 3.00. In the non-heating cases of WSN, there was no growth for  $ky_0 > 1$ , but in experiment 1 there is large growth which must be due in part to the CISK process. The Figure shows that the growth is nearly independent of the scale. Figure 4 contains the amplitudes of  $\psi_T$  and  $\omega_2$  for this experiment.  $\psi_1$  and  $\psi_3$  are not shown for clarity purposes as they have the same magnitude as  $\psi_T$ .  $\psi_1$  is slightly larger and  $\psi_3$  slightly less than  $\psi_T$  but the shape is identical. The units are arbitrary since the basic equations are linear. However,  $\omega_2$  is not plotted on the same scale as  $\psi_T$ . All quantities show double maxima with peaks at  $y = \pm 1.2$ . These results are somewhat similar to those obtained by WSN without heating but their results showed the minimum between peaks as only slightly less than the maximum whereas in Figure 4, the minimum is less than one-half of the maximum. Also the  $\psi_1$ ,  $\psi_3$ , and  $\psi_T$  fields are very close together but WSN showed  $\psi_1$  to be predominate. The closeness of the  $\psi$  fields roughly implies that the vertical mean streamfunction is nearly zero so the fields are basically of a thermal character. Figure 5 contains the phase angles for  $\psi_1$ ,  $\psi_3$ ,  $\psi_T$ , and  $\omega_2$  for this experiment as functions of  $y$ .  $\psi_1$  and  $\psi_T$  are very nearly coincident at the outer edges and  $\psi_1 = \psi_T$  between  $y = \pm 2$  although only  $\psi_1$  is shown in Figure 5.  $\psi_3$  is approximately 180 degrees out-of-phase from  $\psi_1$  and  $\psi_T$  which indicates the pressure trough at the surface is replaced



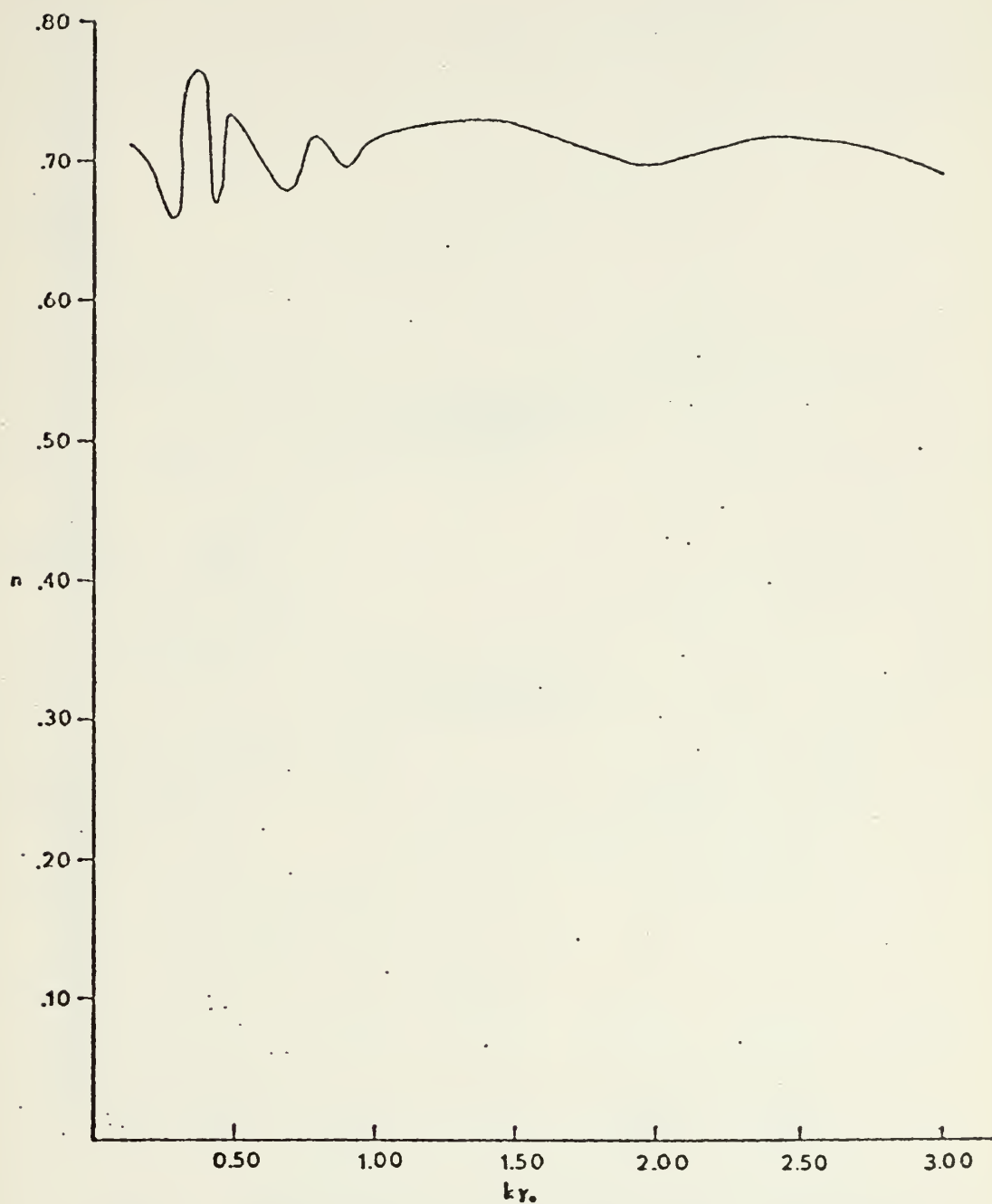


Fig. 3 Growth rates for experiment 1.



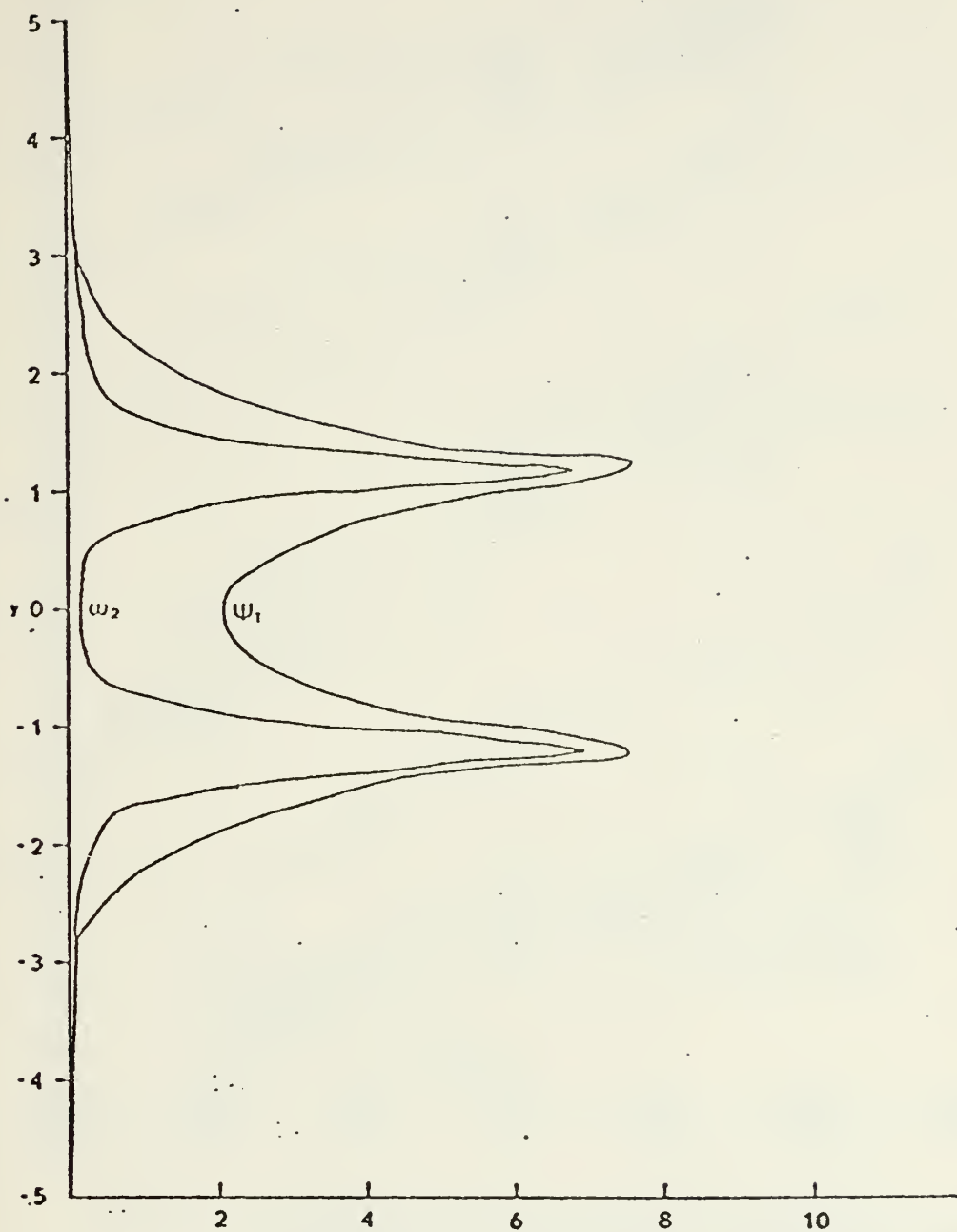


Fig. 4 Amplitudes of  $\psi_T$ , and  $\omega_2$  for experiment 1.  
 $\psi_T$  and  $\omega_2$  are on different scales.



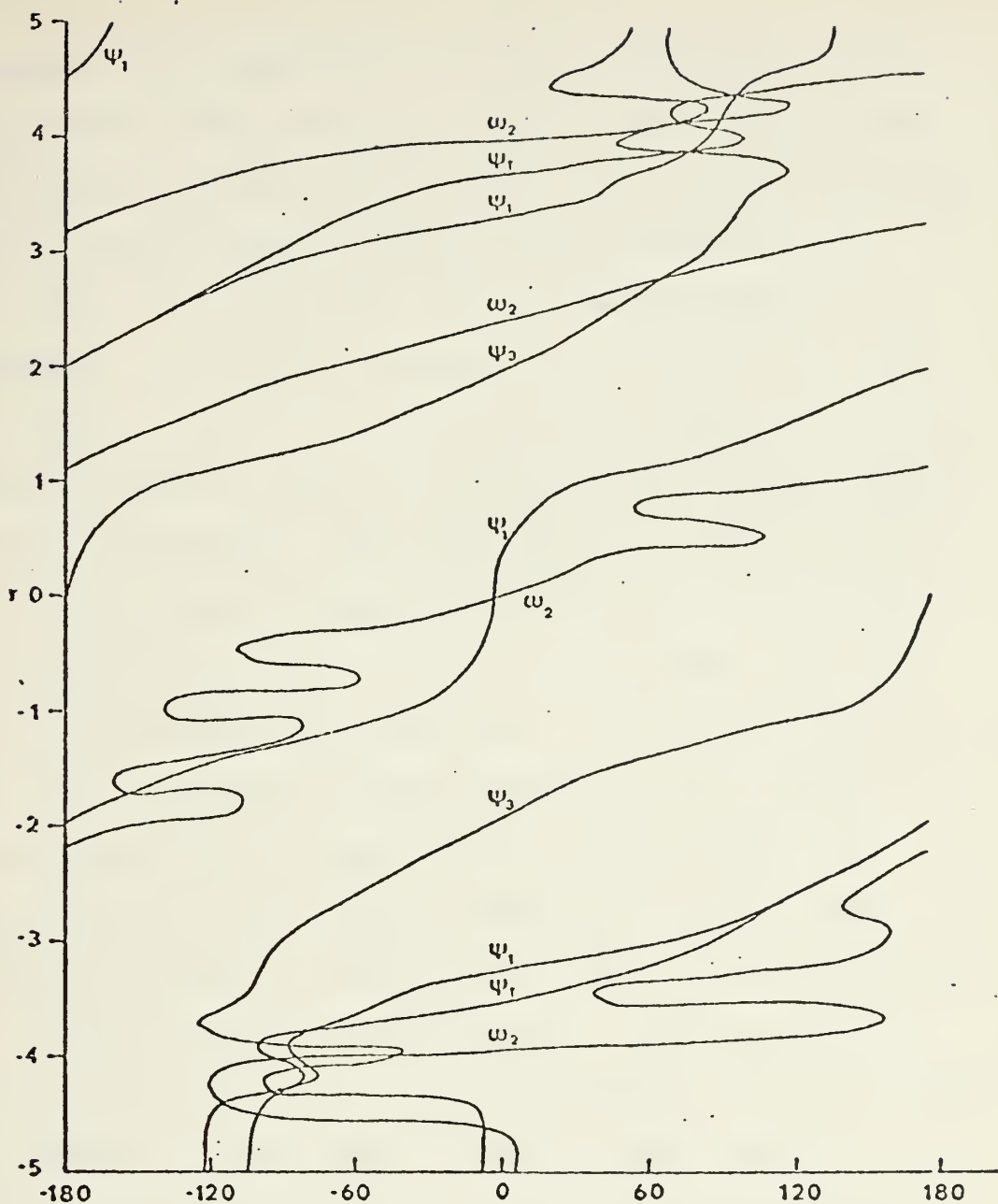


Fig. 5 Phases of  $\psi_1$ ,  $\psi_3$ ,  $\psi_T$ , and  $\omega_2$  for experiment 1 in degrees. Each dependent variable is expressed in the form  $P\cos(kx-\delta)$ , where  $P$  is the amplitude and  $\delta$  is the phase angle.





by a ridge at the upper level. This is consistent because the Ekman effect and heating are tied to the field at level 3 which produces heating above surface low pressure systems. Unlike the results found by WSN for the adiabatic case, Figure 5 shows the horizontal tilt of the disturbance to be a minimum at  $y = 0$  and a maximum at  $y = \pm(1 \text{ to } 4)$ . The general sense of the tilt is northeast but larger than that observed in easterly waves. Also the tilt of the  $\omega_2$  field fluctuates considerably. The small perturbations, particularly in the  $\omega_2$  field, suggest that there is not a clearly defined unstable mode in  $y$ . This does not agree with the results of WSN which had no heating. It is interesting to note that the fields are very smooth but have large gradients except for  $\omega_2$  which shows a radical behavior.

Experiment 2 is the same as experiment 1 except the beta term is included. The results in general are the same. Figure 6 shows the growth rate profile. The magnitude of the growth rates is almost the same although a small decrease in the maximum is noted (from 0.770 to 0.730) and the perturbations between  $ky_0 = 0.10$  and 1.00 have been somewhat smoothed. The maximum growth rate corresponds to a doubling time of 0.44 days and a wave length of 6280 km. Figure 7 contains the amplitudes for experiment 2 as a function of  $y$ . As in experiment 1, only  $\psi_T$  and  $\omega_2$  are shown with  $\psi_T$  and  $\omega_2$  on different scales. Again there is a double maxima at  $y = \pm 1.2$  but the profile is asymmetric with the larger maximum in the shear zone to the north. This asymmetry is



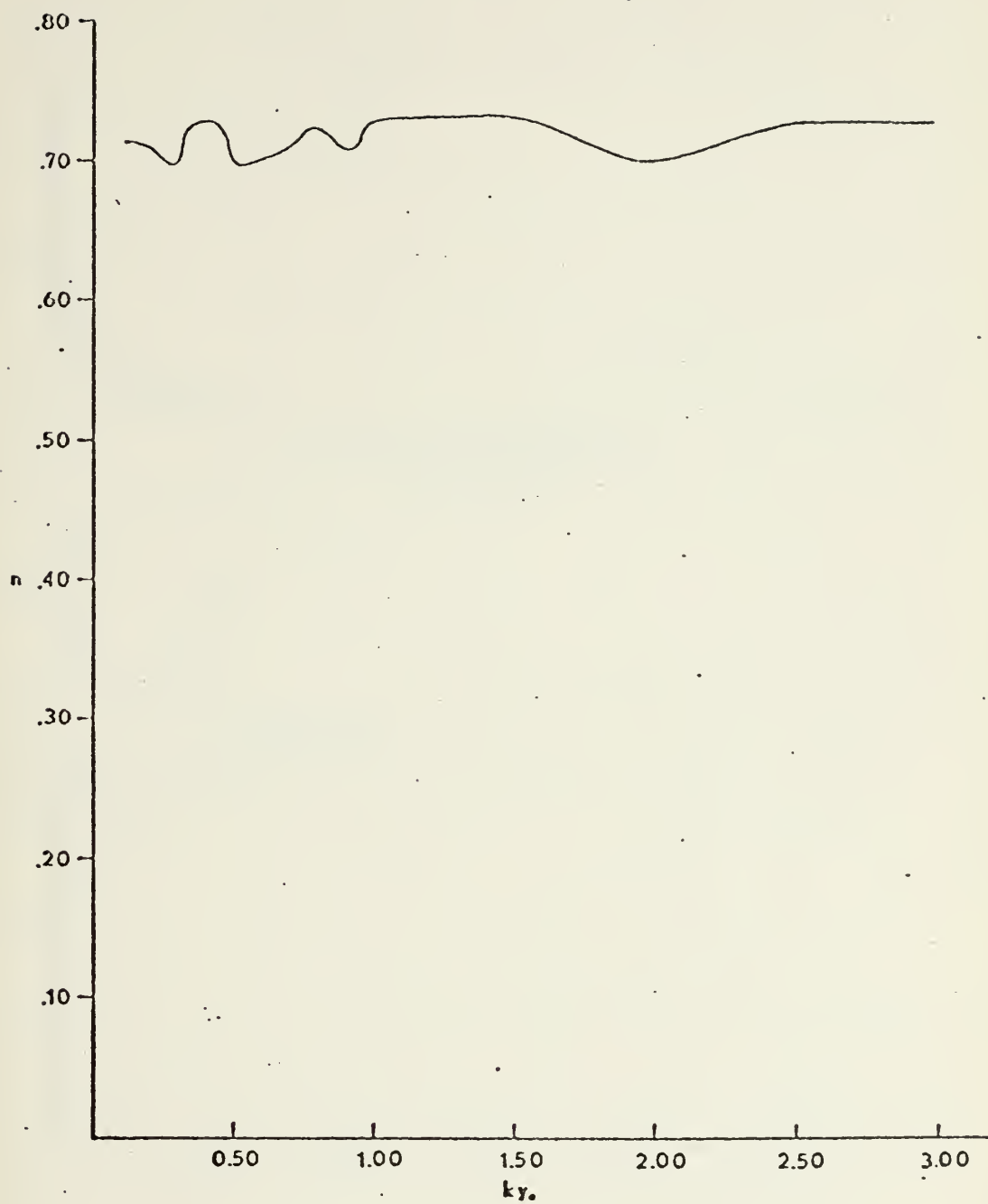


Fig. 6 Growth rates for experiment 2.



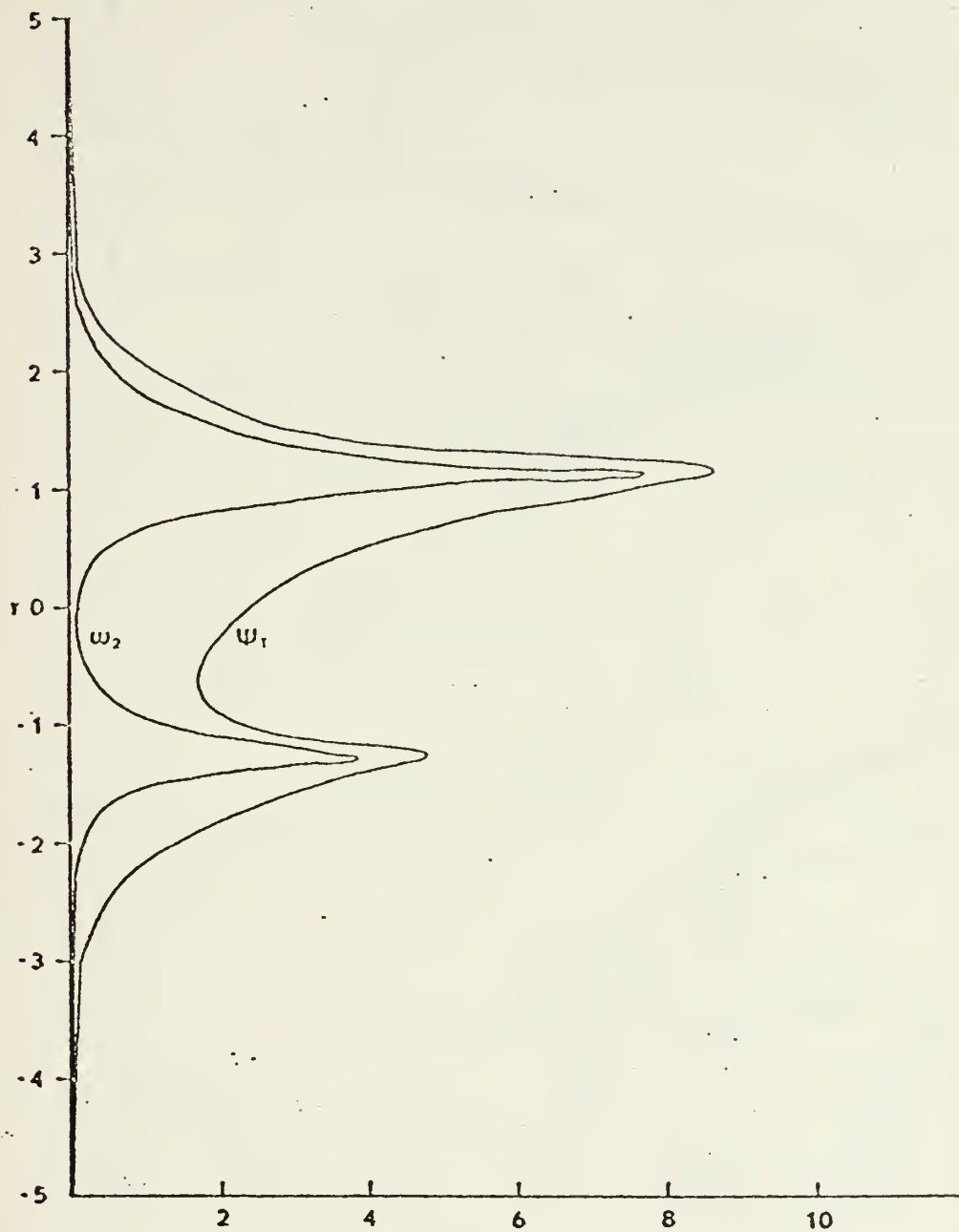


Fig. 7 Amplitudes of  $\psi_T$  and  $\omega_2$  for experiment 2.  
 $\psi_T$  and  $\omega_2$  are on different scales.



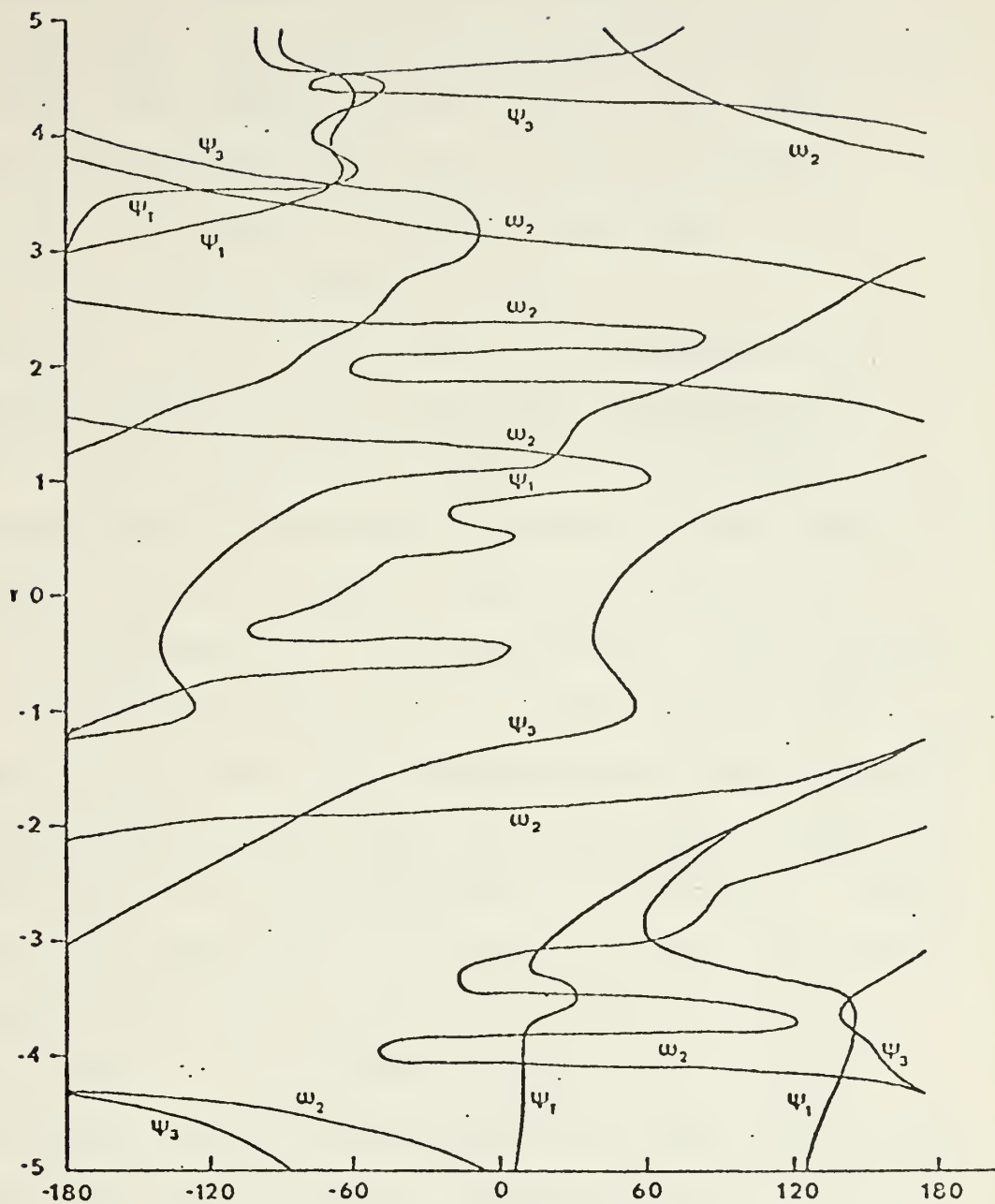


Fig. 8 Phases of  $\psi_1$ ,  $\psi_3$ ,  $\psi_T$ , and  $\omega_2$  for experiment 2 in degrees. Each dependent variable is expressed in the form  $P\cos(kx-\delta)$ , where  $P$  is the amplitude and  $\delta$  is the phase angle.





expected since the absolute vorticity gradient is not an odd function of  $y$ . WSN found that the shift of symmetry was to the south while Figure 7 shows a shift to the north. The phase relationships of  $\psi_1$ ,  $\psi_3$ ,  $\psi_T$ , and  $\omega_2$  shown in Figure 8 are very similar to those in experiment 1 and again only  $\psi_1$  is shown between  $y = \pm 2$ .

Experiment 3 was run with the (4.1) wind profile and included CISK heating, surface friction, and horizontal friction. The beta term was excluded. The horizontal friction was added in an attempt to smooth out the vertical velocity ( $\omega_2$ ) pattern. Figure 9 shows the growth rate profile for experiment 3. The maximum growth rate has been reduced considerably (from 0.770 to 0.520) and the growth falls off at  $ky_0 \geq 2.00$ . The maximum growth rate corresponds to a doubling time of 0.62 days and a wavelength of 6280 km. Note that there are no perturbations in the profile. Figure 10 contains the amplitudes of  $\psi_T$  and  $\omega_2$  for this experiment. As in experiment 1, only  $\psi_T$  and  $\omega_2$  are shown and are on different scales.  $\psi_1$  is slightly larger and  $\psi_3$  slightly smaller than  $\psi_T$ . It is interesting to note that the largest amplitudes are located near the boundaries for all fields whereas in the case without friction (experiment 1), the maximum amplitudes are in the central regions. Perhaps the large scale eddies favored by the horizontal friction are heavily damped by the horizontal shear between  $y = \pm 1$ . Figure 11 contains the phases of  $\psi_1$ ,  $\psi_3$  and  $\omega_2$ .  $\psi_T$  is not shown but it is everywhere equal to  $\psi_1$ . Again  $\psi_T$  and  $\psi_3$



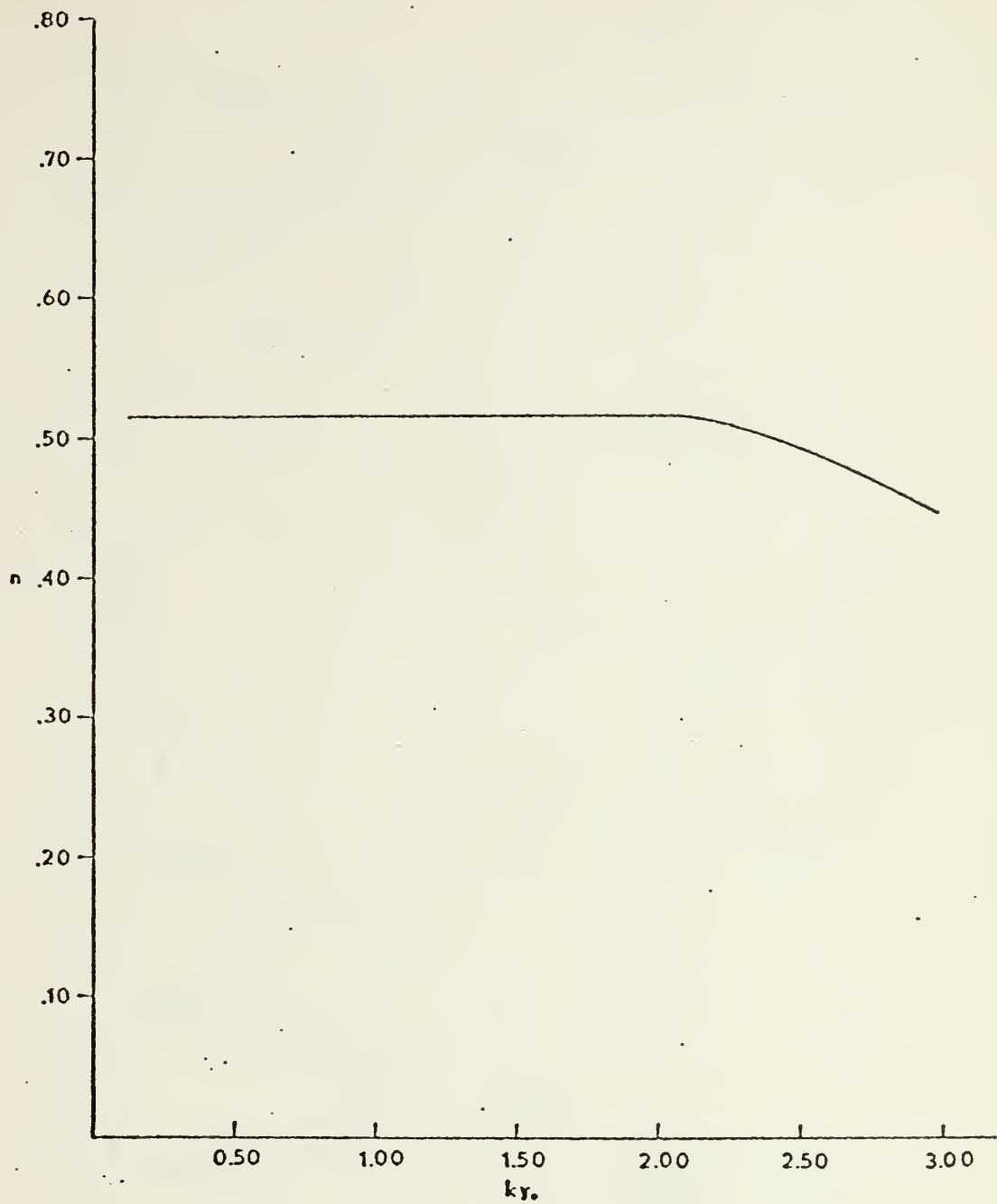


Fig. 9 Growth rates for experiment 3.



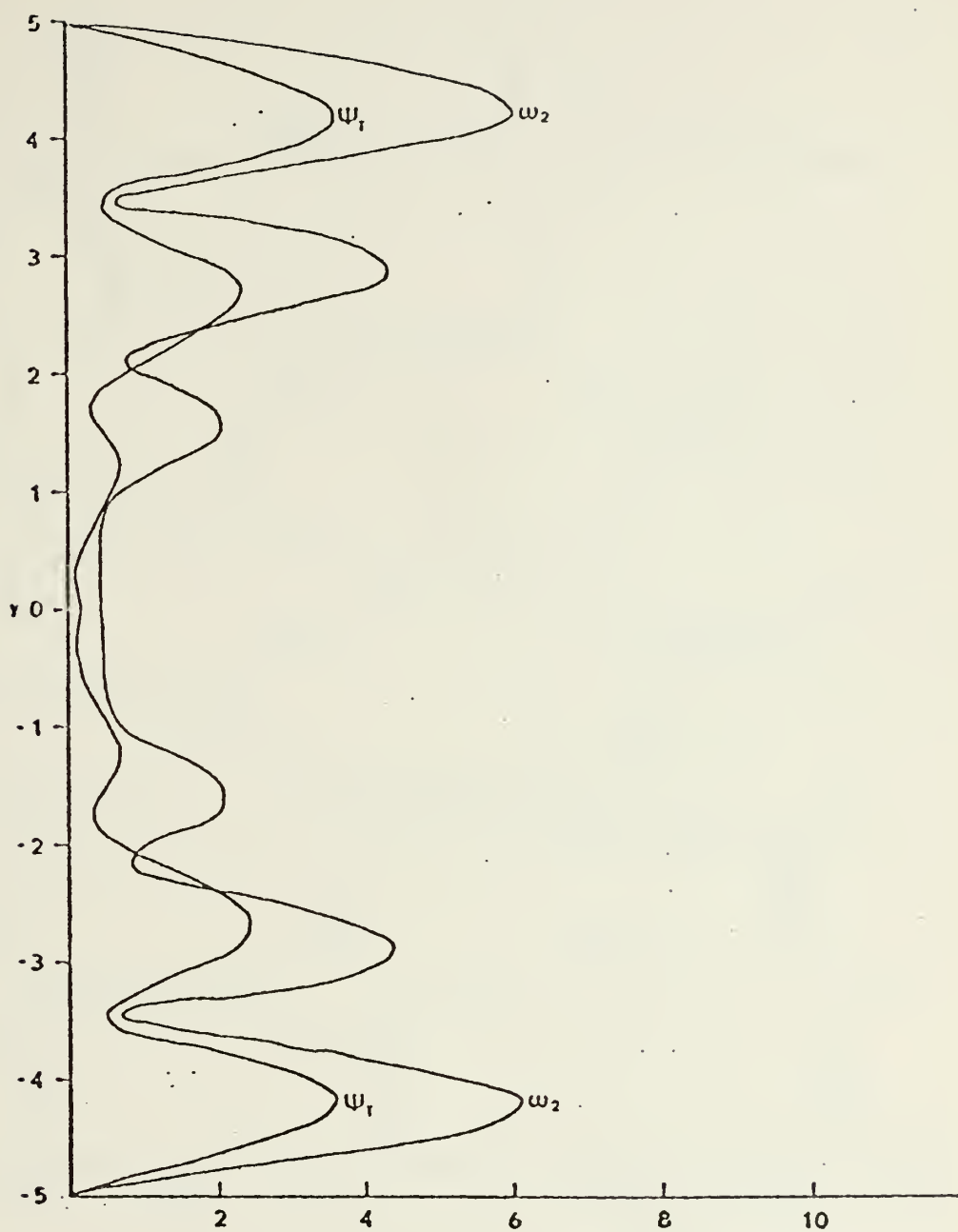


Fig. 10 Amplitudes of  $\psi_T$  and  $\omega_2$  for experiment 3.  
 $\psi_T$  and  $\omega_2$  are on different scales.



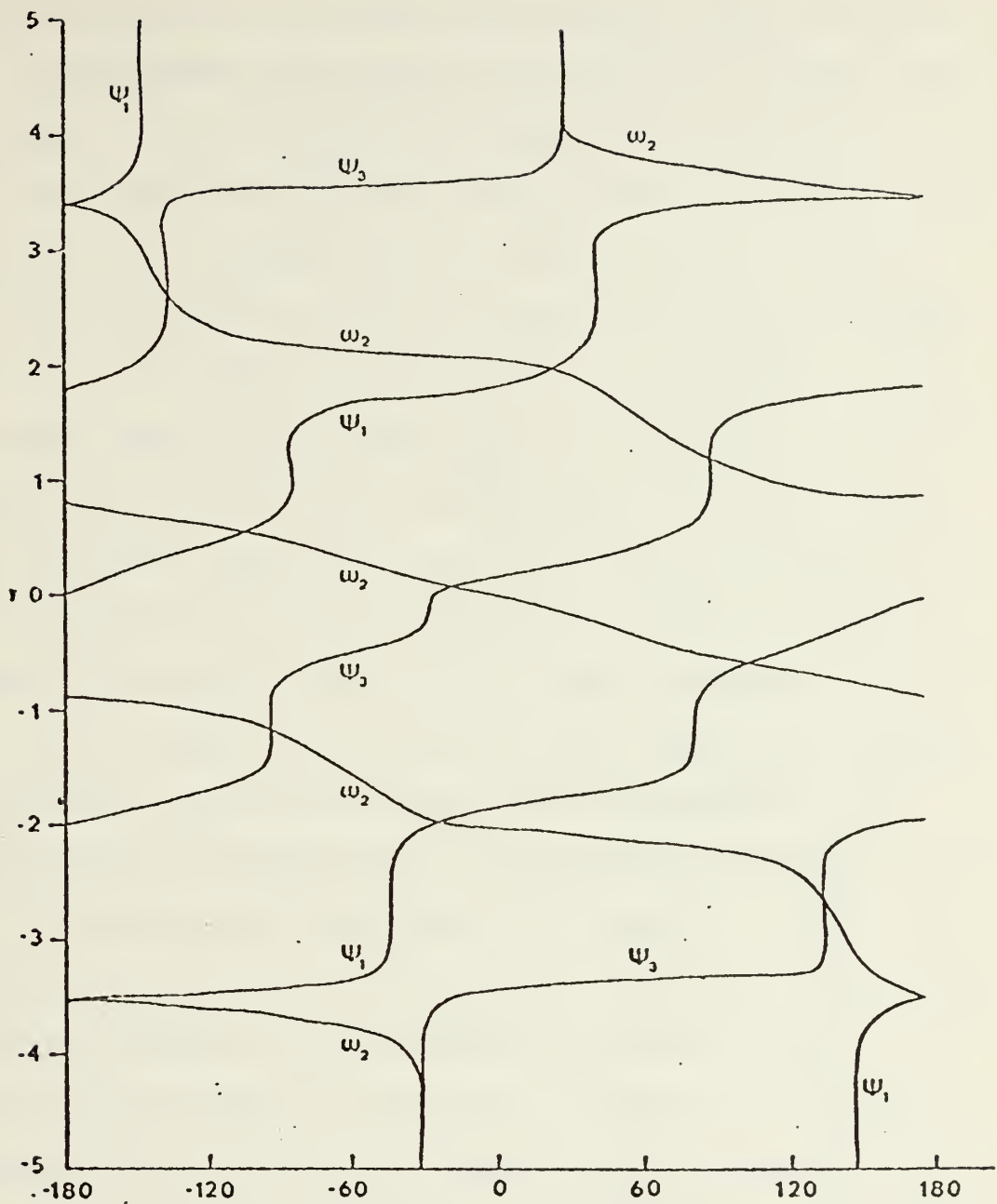


Fig. 11 Phases of  $\psi_1$ ,  $\psi_3$ , and  $\omega_2$  for experiment 3 in degrees. Each dependent variable is expressed in the form  $P\cos(kx-\delta)$ , where  $P$  is the amplitude and  $\delta$  is the phase angle.





are out-of-phase but all fields are smoother than in experiment 1. Where there are peaks in the amplitude fields, the phase angles of  $\omega_2$  and  $\psi_3$  are the same which tends to suggest that warm air is rising and cold air is sinking. Again there is an eastward tilt in the  $\psi$  fields. The  $\omega_2$  field tilt is opposite to the  $\psi$  fields but it does correlate with the  $\psi_3$  field where the amplitude is a maximum. It appears the scale in  $y$  is about  $2y_0$ .

Experiment 4 is the same as experiment 3 but the beta term is included. The beta term has very little effect except to make the solutions asymmetric. Figure 12 shows the growth rate profile which is the same as Figure 9 except for the slight perturbation between the wave numbers 0.40 and 0.90. The maximum growth rate corresponds to a doubling time of 0.62 days and a wavelength of 6280 km. Figure 13 contains the amplitudes of  $\psi_T$  and  $\omega_2$ . As in experiment 3,  $\psi_1$  and  $\psi_3$  are not shown. The only change noted is a slight increase in the maximum to the north and a decrease in the maximum to the south. Figure 14 contains the phases of  $\psi_1$ ,  $\psi_3$  and  $\omega_2$  and again  $\psi_T$  is everywhere equal to  $\psi_1$ . The  $\omega_2$  and  $\psi_3$  correlation is the same as in experiment 3.

Experiment 5 was run with (4.2) wind profile and surface friction. Heating and horizontal friction were excluded. This profile is a mirror reflection of the  $\bar{U}_1$  profile, that is  $-\bar{U}_1$ . This profile is similar in general to the wind profile in the Intertropical Convergence Zone where there



is cyclonic shear in the lower region and anticyclonic shear in the upper region. Since the ITCZ is driven by heating and convergence, this is the type of mean wind pattern that is expected. Three cases were run although only one is shown in the table. Case 1, which is summarized in Table 1, had a grid mesh of 50 km, a  $y_0$  value of 400 km and a time step of 1.0 hours. Case 2 used a grid mesh of 25 km, a  $y_0$  value of 200 km and a time step of 0.50 hours. Case 3 used a grid mesh of 12.5 km, a  $y_0$  value of 100 km and a time step of 0.25 hours. Case 1 was run over the range of wave numbers from 0.10 to 1.20 and the maximum unstable mode was found at  $ky_0 = 0.65$ . Cases 2 and 3 were run only at wave number 0.65. Figure 15 shows the growth rate profile for experiment 5, case 1. The maximum growth rate at  $ky_0 = 0.65$  was 0.283. The doubling time was 1.13 days with a wavelength of 3465 km. For case 2, the growth rate obtained was 0.188 with a doubling time of 0.85 days and a 1930 km wavelength. For case 3 a growth rate of 0.162 was found with a doubling time of 0.50 days and a 967 km wavelength. For cases 2 and 3,  $ky_0 = 0.65$  may not be the maximum growth rate. This shows that as the scale ( $y_0$ ) is decreased, the baroclinic process is suppressed. This is consistent with baroclinic instability theory. It is noted that in case 3, the growth rate is the same as that obtained by WSN in their experiment 1. Figure 16 contains the amplitudes of  $\psi_1$ ,  $\psi_T$  and  $\omega_2$  for case 1. For clarity,  $\psi_3$  is not shown but it is slightly less than  $\psi_1$ . These amplitudes are very similar to those of WSN



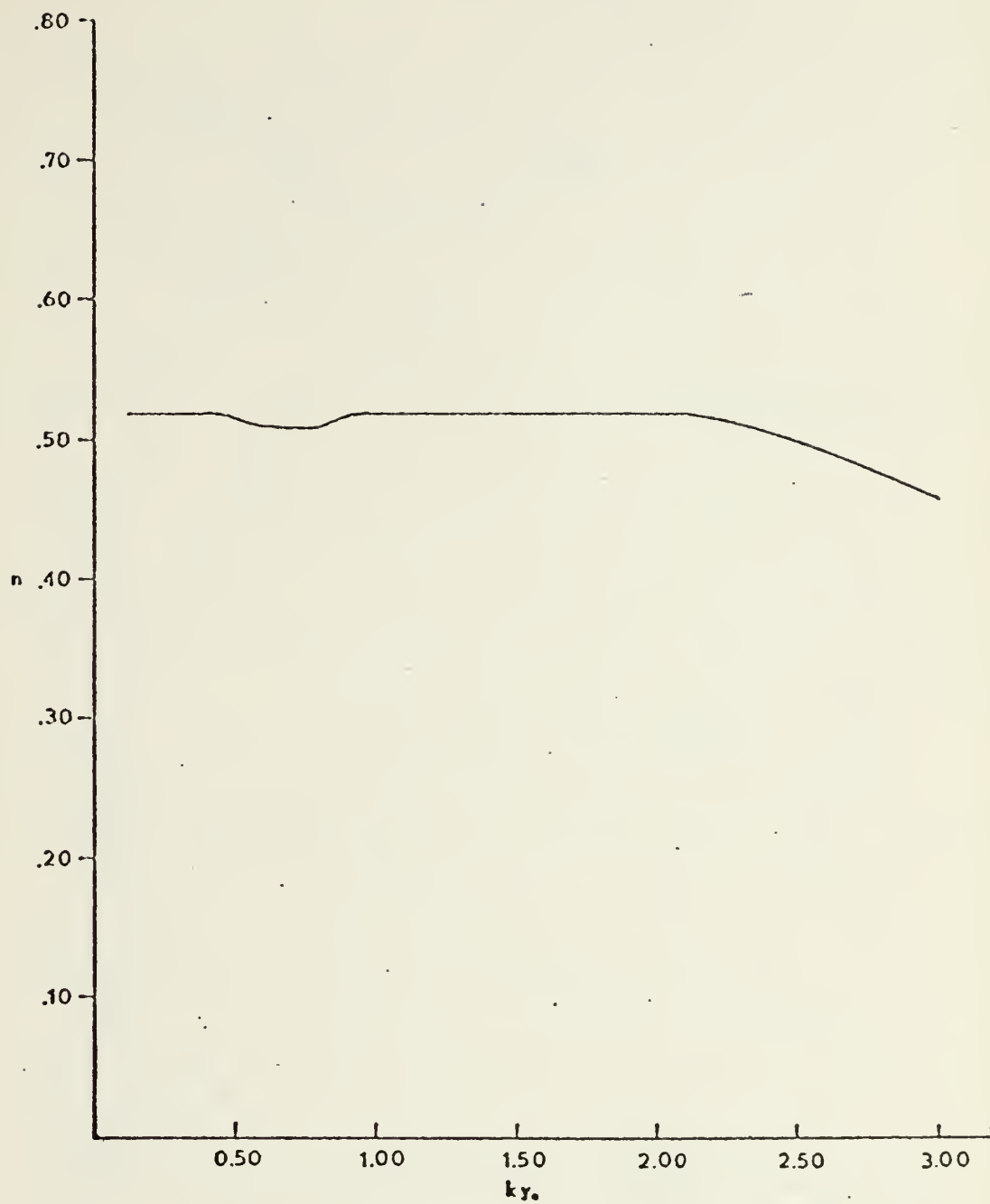
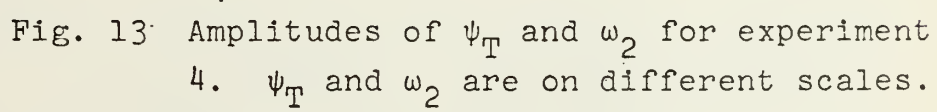


Fig. 12 Growth rates for experiment 4.









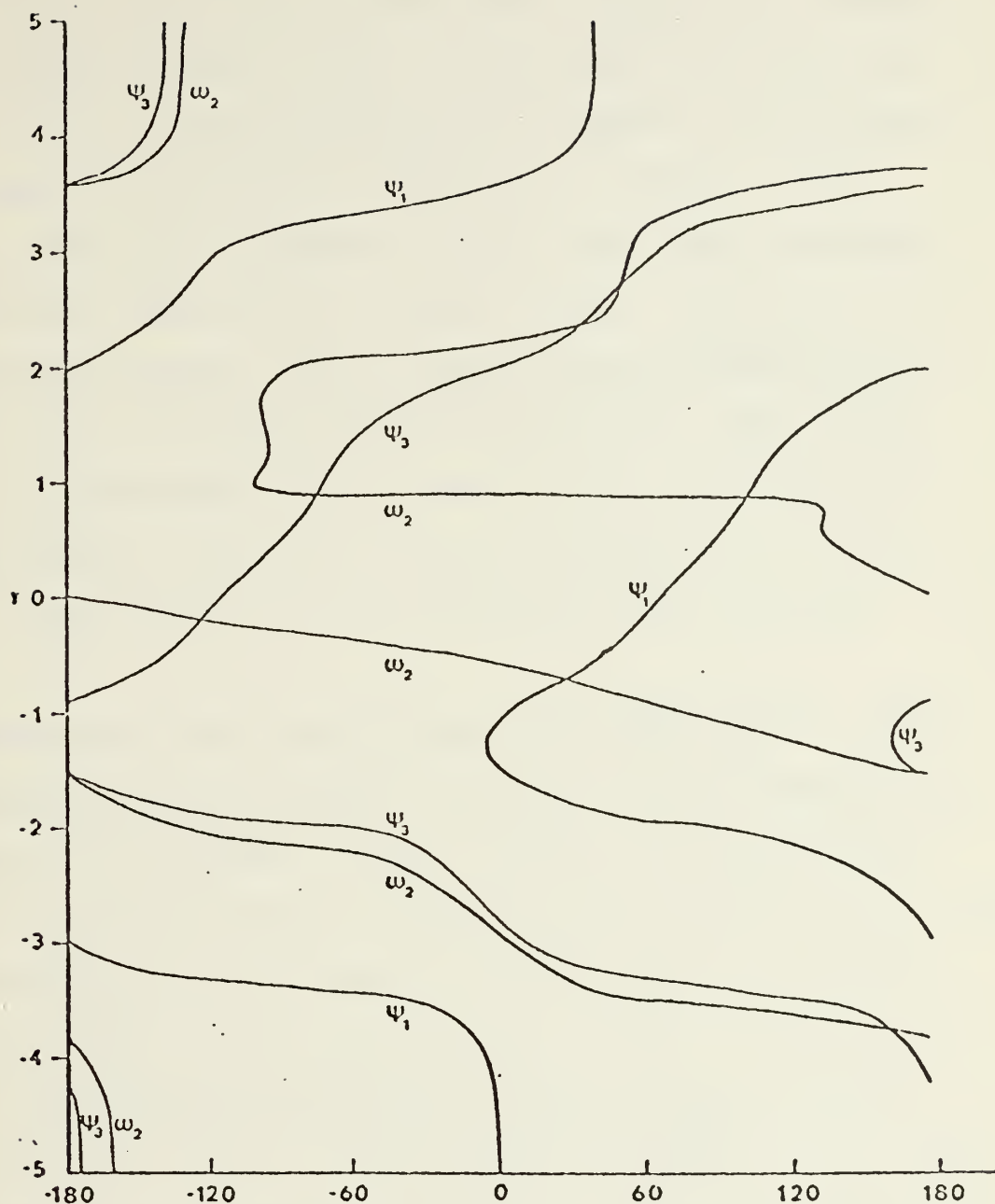


Fig. 14 Phases of  $\psi_1$ ,  $\psi_3$ , and  $\omega_2$  for experiment 4 in degrees. Each dependent variable is expressed in the form  $P\cos(kx-\delta)$ , where  $P$  is the amplitude and  $\delta$  is the phase angle.



in their Figure 4A. The amplitudes for cases 2 and 3 are not shown but they are much the same as Figure 16. Figure 17 contains the phases of  $\psi_1$ ,  $\psi_3$ ,  $\psi_T$ , and  $\omega_2$  as functions of  $y$ .  $\psi_T$  and  $\omega_2$  are approximately 165 degrees out-of-phase. This implies a baroclinic conversion of kinetic energy. However, the tilt is opposite to the shear which indicates a barotropic conversion of kinetic energy. The tilt is westward with height north of the ITCZ and eastward with height south of the ITCZ which is consistent with rising motion and unsettled weather that is often observed east of the surface trough axis in easterly waves north of the ITCZ. These results are also consistent with those of WSN.

Experiment 6 was run with the (4.2) wind profile, CISK heating and surface friction. The beta term and horizontal friction were excluded. Figure 18 shows the growth rates for this experiment with a maximum unstable mode at  $ky_0 = 1.10$  corresponding to a doubling time of 0.41 days and a wavelength of 2285 km. The growth rate of 0.790 is similar to that of experiment 1 and again the large value was due to the large value of  $\eta$ . The perturbations between wave numbers 0.10 and 1.10 are even larger than in experiment 1 indicating that there is no clearly defined unstable mode in  $y$ . The amplitudes have a pattern similar to Figure 4. The phases for this experiment tilted northeast as in the other cases.



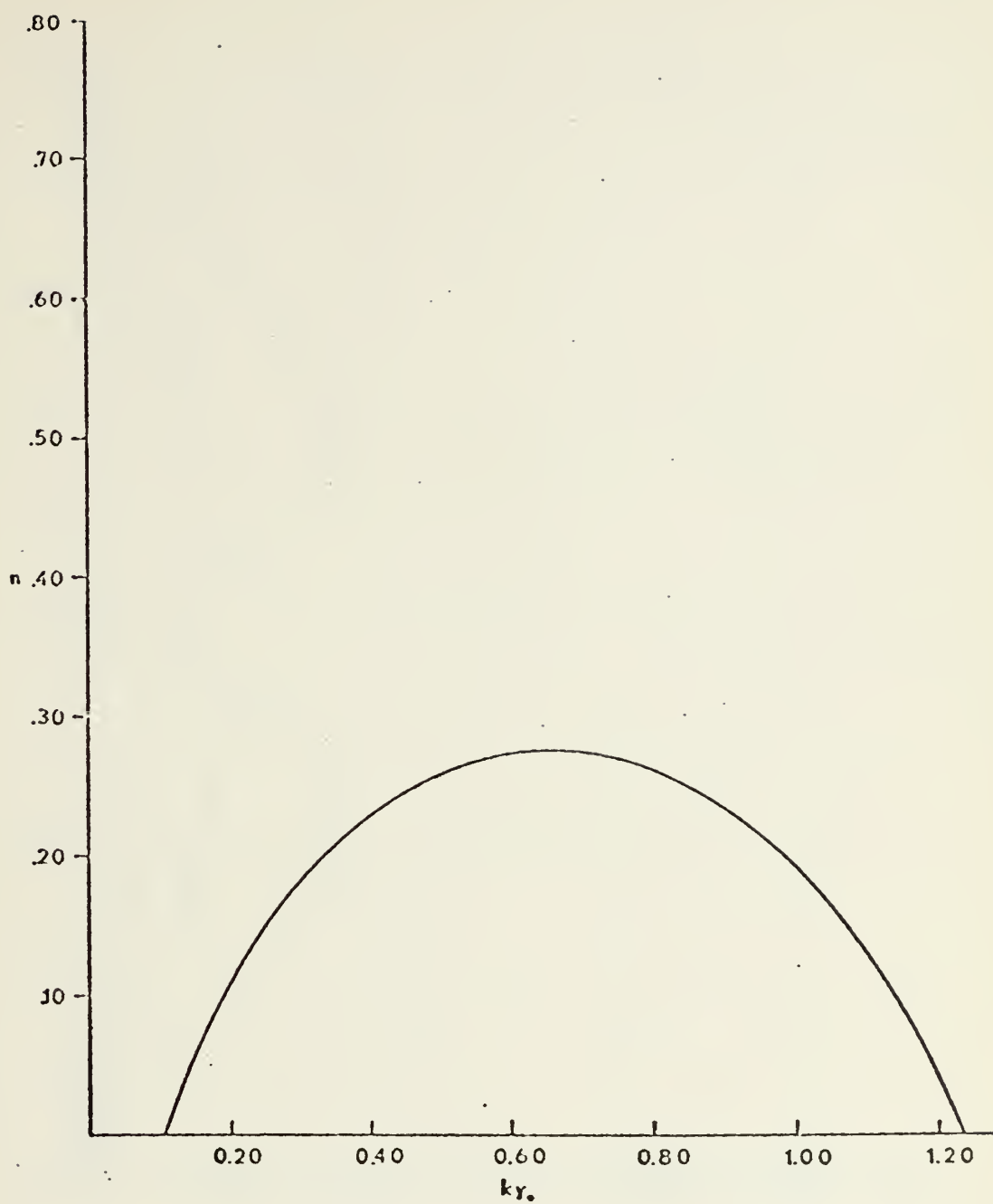


Fig. 15 Growth rates for experiment 5, case 1.



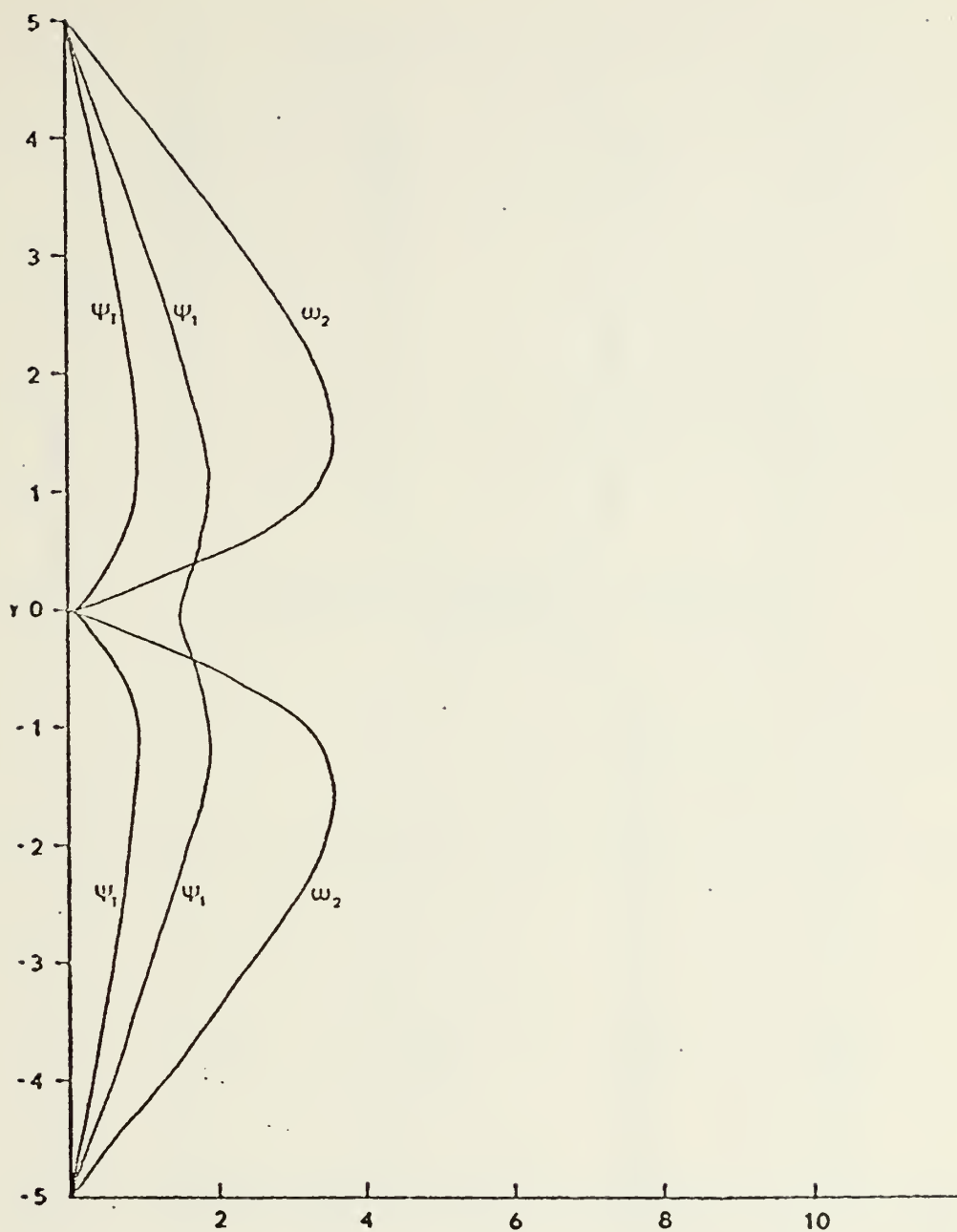


Fig. 16 Amplitudes of  $\psi_1$ ,  $\psi_T$ , and  $\omega_2$  for experiment 5, case 1. The quantities  $\psi_1$  and  $\psi_T$  have the same scale;  $\omega_2$  is on a different scale.





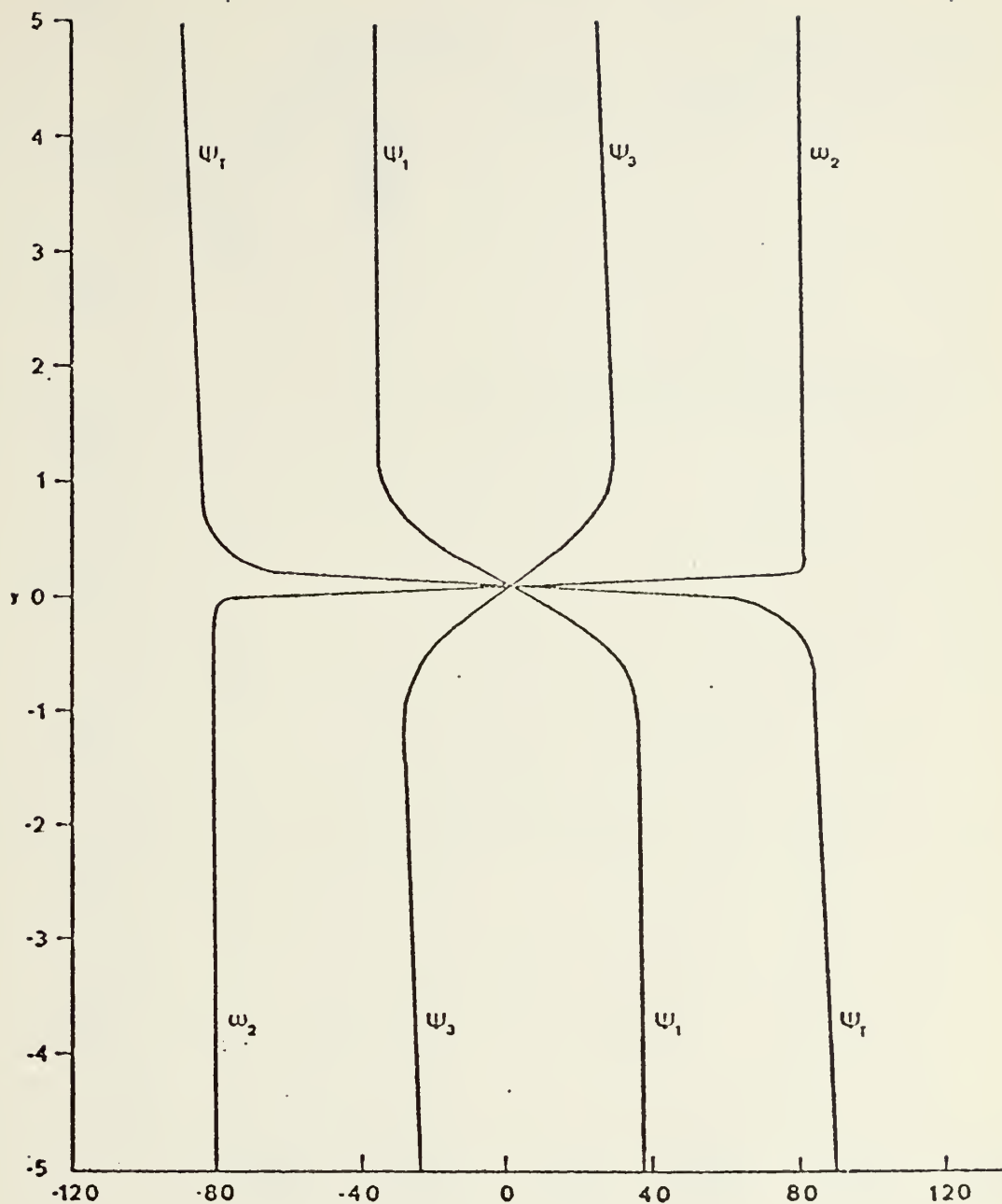


Fig. 17 Phases of  $\psi_1$ ,  $\psi_3$ ,  $\psi_T$ , and  $\omega_2$  for experiment 5, case 1 in degrees. Each dependent variable is expressed in the form  $P\cos(kx-\delta)$ , where  $P$  is the amplitude and  $\delta$  is the phase angle.



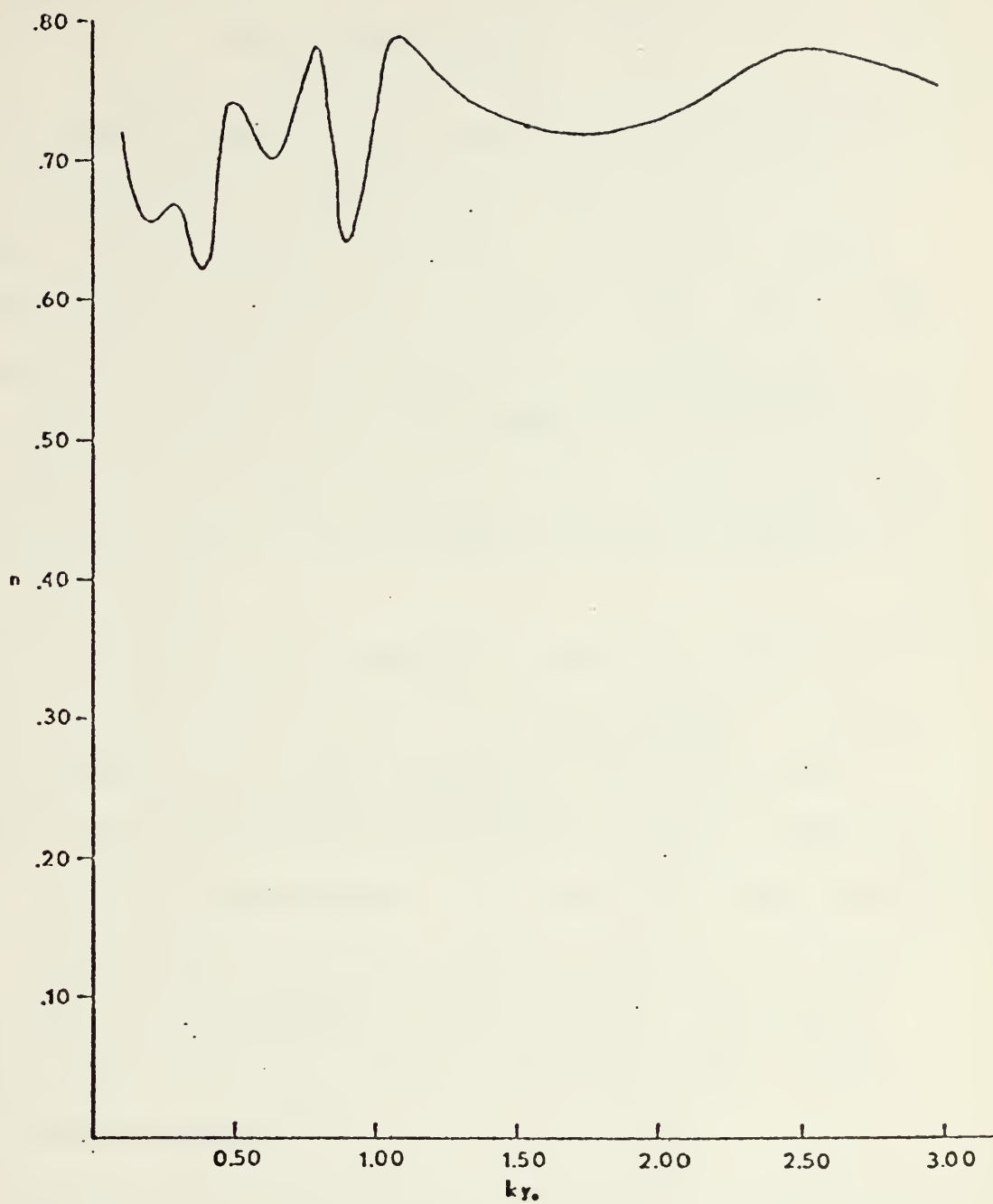


Fig. 18 Growth rates for experiment 6.



## VII. CONCLUSIONS

In this thesis, numerically computed barotropically unstable disturbances are compared with tropospheric waves that occur in the tropical easterlies. A two-level quasi-geostrophic model is used with an attached Ekman layer. The most unstable solutions are obtained numerically by the initial value procedure. Two basic shear zone profiles are used: (1)  $\bar{U}_1 = \bar{U}_3 = -U_0 \tanh y/y_0$  and (2)  $\bar{U}_1 = -\bar{U}_3 = U_0 \tanh y/y_0$ . Calculations were made in which CISK heating and horizontal friction were added.

Certain features of the predicted wave structures do correspond to observed tropical wave disturbances. The tilt of the disturbance in a sense opposite to the horizontal wind shear that was observed by Wallace and Chang (1969) is present in all the experiments. All experiments which contain heating have the warm structure which was observed by Chang et al. (1970). The presence of rising motion to the east of the wave axis which was noted by Yanai and Nitta (1967) is observed in experiment 5.

The growth rates obtained with heating are unrealistically large, but it was shown that these could be greatly reduced by choosing a smaller value of the parameter  $\eta$ . It was also noted that when heating is present there is no truly preferred scale of instability. This has been observed by Chang (1971). It was pointed out in the Introduction that,



while mature tropical wave disturbances may be driven by CISK heating, they may originate from barotropic instability (Bates 1970). If so, then the disturbance should retain certain features (latitude structure, wavelength, etc.) of the barotropically unstable modes. This would provide a selection process which does not occur if CISK heating is present from the start.

The studies of this thesis should be continued but a more complicated model is needed. Proper parameterization of the heating term is necessary. A primitive equation model which includes a better treatment of the boundary layer should be used.





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## DOCUMENT CONTROL DATA - R &amp; D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

ORIGINATING ACTIVITY (Corporate author) Naval Postgraduate School Monterey, California 93940		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
REPORT TITLE  Stability of a Tropical Model Including Shear, Surface Friction and CISK Heating			
1. DESCRIPTIVE NOTES (Type of report and, inclusive dates) Master's Thesis; March 1973			
3. AUTHOR(S) (First name, middle initial, last name)  Terry G. Robertson			
REPORT DATE March 1973	7a. TOTAL NO. OF PAGES 62	7b. NO. OF REFS 29	
2. CONTRACT OR GRANT NO.	9a. ORIGINATOR'S REPORT NUMBER(S)		
b. PROJECT NO.			
c.	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)		
d.			
10. DISTRIBUTION STATEMENT  Approved for public release; distribution unlimited.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Naval Postgraduate School Monterey, California 93940	
13. ABSTRACT  The structure of barotropically unstable disturbances in the tropics is studied with a two-level quasi-geostrophic model. An Ekman layer is attached to the lower boundary. The equations are linearized and the most unstable mode is found numerically by use of the initial value technique. CISK heating, horizontal friction and shear are introduced to give more realistic solutions. Computations are made for two shear zone wind profiles. The first is represented by $\bar{U}_1 = \bar{U}_3 = -U_0 \tanh y/y_0$ and the second is a mirror reflection of the first and is given by $\bar{U}_3 = -\bar{U}_1$ . The model is run for 142 days after which growth rates are determined as a function of the non-dimensional wave number $ky_0$ . The associated phase angles and amplitudes for the wave numbers with maximum growth rates are given. The solutions with heating do not have a strongly preferred mode of maximum growth.			



## KEY WORDS

## LINK A

## LINK B

## LINK C

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Barotropic instability

Two-level model

CISK heating

Horizontal friction

Tropical disturbances

Vertical shear





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